

**A COMPUTATIONALLY PRACTICAL  
INTERIOR-POINT TRUST-REGION  
ALGORITHM FOR SOLVING THE  
GENERAL NONLINEAR PROGRAMMING  
PROBLEMS**

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**Abstract**

An interior-point trust-region algorithm for solving the general nonlinear programming problem is proposed. In the algorithm, an interior-point Newton method with Coleman-Li scaling matrix is used. A trust-region globalization strategy is added to the algorithm to insure global convergence. A projected Hessian technique is used to simplify the trust-region subproblems.

A Matlab implementation of the algorithm was used and tested against some existing codes. In addition, four case studies were presented to test the performance of the proposed algorithm. The results showed that the algorithm out perform some existing methods in literature.

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**Key words:** Newton's method, interior-point, trust-region, projected-Hessian, nonlinear programming, Matlab implementations, numerical comparisons, case study.

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## 1 Introduction

Various approaches have been proposed and used to solve the following general nonlinear programming problem

$$\begin{aligned} & \text{minimize} && f(x) \\ & \text{subject to} && C(x) = 0, \\ & && a \leq x \leq b, \end{aligned} \tag{1.1}$$

where  $f : \mathfrak{R}^n \rightarrow \mathfrak{R}$ ,  $C : \mathfrak{R}^n \rightarrow \mathfrak{R}^m$ ,  $a \in \{\mathfrak{R} \cup \{-\infty\}\}^n$ ,  $b \in \{\mathfrak{R} \cup \{+\infty\}\}^n$ ,  $m < n$ , and  $a < b$ . We assume that the functions  $f$  and  $C$  are at least twice continuously differentiable.

The Lagrangian function associated with Problem (1.1) is given by

$$L(x, \lambda, \mu, \nu) = \ell(x, \lambda) - \mu^T(x - a) - \nu^T(b - x), \tag{1.2}$$

where  $\ell(x, \lambda) = f(x) + \lambda^T C(x)$  and  $\lambda$ ,  $\mu$ , and  $\nu$  are the Lagrange multiplier vectors associated with the equality constraint  $C(x) = 0$ , and the inequality constraints  $(x - a) \geq 0$  and  $(b - x) \geq 0$  respectively.

The first-order necessary conditions for a point  $x_*$  to be a solution of problem (1.1) are the existence of multipliers  $\lambda_* \in \mathfrak{R}^m$ ,  $\mu_* \in \mathfrak{R}_+^n$ , and  $\nu_* \in \mathfrak{R}_+^n$ , such that  $(x_*, \lambda_*, \mu_*, \nu_*)$  satisfies

$$\nabla_x \ell(x_*, \lambda_*) - \mu_* + \nu_* = 0, \tag{1.3}$$

$$C(x_*) = 0, \tag{1.4}$$

$$a \leq x_* \leq b, \tag{1.5}$$

and for all  $i$  corresponding to  $x^{(i)}$  with finite bound, we have

$$\mu_*^{(i)}(x_*^{(i)} - a^{(i)}) = 0, \tag{1.6}$$

$$\nu_*^{(i)}(b^{(i)} - x_*^{(i)}) = 0, \tag{1.7}$$

In addition to that, for any  $i$  corresponding to  $x^{(i)}$  with infinite bound the corresponding  $\mu_*^{(i)}$  or  $\nu_*^{(i)}$  is zero.

Motivated by the strategy in [12], we define the diagonal scaling matrix  $D(x)$  whose diagonal elements are given by

$$d^{(i)}(x) = \begin{cases} \sqrt{(x^{(i)} - a^{(i)})}, & \text{if } \nabla_x \ell(x, \lambda) \geq 0 \text{ and } a^{(i)} > -\infty, \\ \sqrt{(b^{(i)} - x^{(i)})}, & \text{if } \nabla_x \ell(x, \lambda) < 0 \text{ and } b^{(i)} < +\infty, \\ 1, & \text{otherwise.} \end{cases} \tag{1.8}$$

The scaling matrix  $D(x)$  was first introduced in [6] for unconstrained optimization problem with simple bound and was used by [7], [12],[13].

Using the scaling matrix  $D(x)$ , the first-order necessary conditions (1.3)-(1.7) are equivalent to the following conditions

$$D^2(x)\nabla_x\ell(x, \lambda) = 0, \quad (1.9)$$

$$C(x) = 0, \quad (1.10)$$

$$a \leq x \leq b. \quad (1.11)$$

By applying Newton's method on the nonlinear system (1.9),(1.10), we obtain

$$[D^2(x)\nabla_x^2\ell(x, \lambda) + \text{diag}(\nabla_x\ell(x, \lambda))\text{diag}(\eta(x))]\Delta x \quad (1.12)$$

$$+ D^2(x)\nabla C(x)\Delta\lambda = -D^2(x)\nabla_x\ell(x, \lambda),$$

$$\nabla C(x)^T\Delta x = -C(x), \quad (1.13)$$

where  $\eta^{(i)}(x) = \frac{\partial((d^{(i)}(x))^2)}{\partial x^{(i)}}$ ,  $i = 1, \dots, n$ . More details about the derivation of equations (1.13) is given in [7],[12].

Enforcing  $a < x < b$  makes  $D(x)$  nonsingular. Now multiplying both sides of Equation (1.13) by  $D^{-1}(x)$ , we obtain

$$[D(x)\nabla_x^2\ell(x, \lambda) + D^{-1}(x)\text{diag}(\nabla_x\ell(x, \lambda))\text{diag}(\eta(x))]\Delta x$$

$$+ D(x)\nabla C(x)\Delta\lambda = -D(x)\nabla_x\ell(x, \lambda),$$

$$\nabla C(x)^T\Delta x = -C(x).$$

If we scale the step using  $\Delta x = D(x)s$ , the above system will have the form

$$Bs + D(x)\nabla C(x)\Delta\lambda = -D(x)\nabla_x\ell(x, \lambda), \quad (1.14)$$

$$(D(x)\nabla C(x))^T s = -C(x). \quad (1.15)$$

where

$$B = D(x)\nabla_x^2\ell(x, \lambda)D(x) + \text{diag}(\nabla_x\ell(x, \lambda))\text{diag}(\eta(x)).$$

The above system shares the advantages and the disadvantages of Newton's method. From Newton's good side, under the standard assumptions for Newton's method for problem (1.1), the method converges quadratically to a stationary point  $(x_*, \lambda_*)$  [12]. On the other side, it has the disadvantage of local convergence. This means that the starting point  $(x_0, \lambda_0)$  must be sufficiently closed to  $(x_*, \lambda_*)$  in order to guarantee convergence. In other words, it may not converge at all if the starting point is far away from the solution.

Trust-region approach is a very successful approach to insure global convergence from any starting point, see [6],[11]. To add a trust-region constraint, we have to rewrite the extended system (1.14)-(1.15) as a minimization problem. An equivalent problem is the following quadratic programming problem

$$\begin{aligned} & \text{minimize} && (D\nabla_x\ell)^T s + \frac{1}{2}s^T Bs \\ & \text{subject to} && (D\nabla C)^T s + C = 0 \end{aligned} \quad (1.16)$$

Notice that the first order necessary conditions of problem (1.16) coincides with (1.14)-(1.15).

If a trust-region constraint is simply added to Problem (1.16), the resulting problem will take the form

$$\begin{aligned} & \text{minimize} && (D_k \nabla_x \ell_k)^T s + \frac{1}{2} s^T B_k s \\ & \text{subject to} && (D_k \nabla C_k)^T s + C_k = 0, \\ & && \|s\|_2 \leq \delta_k. \end{aligned} \quad (1.17)$$

But this trust-region subproblem may be infeasible because the intersecting points between the trust-region constraint and the hyperplane of the linearized constraints may not exist. Even if they intersect, there is no guarantee that the intersecting set will remain nonempty if the trust-region radius is decreased.

The reduced Hessian is a successful approach to overcome the difficulty of having a possible infeasible trust-region subproblem. This approach was suggested by Byrd [4] and Omojokun [19].

The following notations are used throughout the rest of the paper. A subscripted function means the value of the function evaluated at a particular point. For example,  $f_k \equiv f(x_k)$ ,  $C_k \equiv C(x_k)$ ,  $D_k \equiv D_k(x_k)$  and so on. We use the notation  $\nabla_x \ell_k^{(i)}$  to denote the  $i$ th component of the vector  $\nabla_x \ell_k$  and  $x_k^{(i)}$  to denote the  $i$ th component of the vector  $x_k$ , and so on. Finally, all norms used in this paper are  $\ell_2$ -norms.

The paper is organized as follows. In section 2, a detailed description of the main steps of the interior-point trust-region Algorithm IPTRA is given. Section 3 contains a Matlab implementation and reports of the numerical results of Algorithm IPTRA. Section 4 contains four case studies of Algorithm IPTRA. Finally, Section 5 contains some concluding remarks.

## 2 Description of the Algorithm

In this section a detailed description of the proposed interior-point trust-region algorithm (IPTRA) for solving problem (1.1) is given.

### 2.1 Computing a trial step

The reduced-Hessian approach is used to compute a trial step  $s_k$ . In this approach, the trial step  $s_k$  is decomposed into two orthogonal components; the normal component  $s_k^n$  and the tangential component  $s_k^t$ . The trial step  $s_k$  has the form  $s_k = s_k^n + Z_k s_k^t$ , where  $Z_k$  is a matrix whose columns form an orthonormal basis for the null space of  $(D_k \nabla C_k)^T$ .

We obtain the normal component  $s_k^n$  by solving the following trust-region subproblem

$$\begin{aligned} & \text{minimize} && \frac{1}{2} \|(D_k \nabla C_k)^T s^n + C_k\|^2 \\ & \text{subject to} && \|s^n\| \leq \zeta \delta_k, \end{aligned} \quad (2.1)$$

for some  $\zeta \in (0, 1)$ , where  $\delta_k$  is the trust-region radius.

Given the normal component  $s_k^n$ , the step  $\bar{s}_k^t$  is computed by solving the following trust-region subproblem

$$\begin{aligned} & \text{minimize} && [Z_k^T(D_k \nabla_x \ell_k + B_k s_k^n)]^T \bar{s}^t + \frac{1}{2} \bar{s}^{tT} Z_k^T B_k Z_k \bar{s}^t \\ & \text{subject to} && \|Z_k \bar{s}^t\| \leq \Delta_k, \end{aligned} \quad (2.2)$$

where  $\Delta_k = \sqrt{\delta_k^2 - \|s_k^n\|^2}$ . Once the step  $\bar{s}_k^t$  is computed, the tangential component  $s_k^t$  is given by  $s_k^t = Z_k \bar{s}_k^t$ . To solve the trust-region subproblems (2.1) and (2.2) we use the dogleg algorithm.

Having computed the trial step  $s_k$ , the scaled step  $\Delta x_k = D_k s_k$ , is computed. A damping parameter  $\tau_k$  is needed to ensure that the new point  $x_k + \Delta x_k$  lies inside the box constraint. It is computed using the following Scheme:

**Scheme 2.1.** (computing  $\tau_k$ )

$$\text{Compute } u_k^{(i)} = \begin{cases} \frac{a^{(i)} - x_k^{(i)}}{\Delta x_k^{(i)}}, & \text{if } a^{(i)} > -\infty \text{ and } \Delta x_k^{(i)} < 0 \\ 1, & \text{otherwise,} \end{cases}$$

$$\text{Compute } v_k^{(i)} = \begin{cases} \frac{b^{(i)} - x_k^{(i)}}{\Delta x_k^{(i)}}, & \text{if } b^{(i)} < \infty \text{ and } \Delta x_k^{(i)} > 0 \\ 1, & \text{otherwise.} \end{cases}$$

$$\text{Set } \tau_k = \min\{1, \min_i \{u_k^{(i)}, v_k^{(i)}\}\}$$

Since it is always require that  $\{x_k\}$  satisfy, for all  $k$ ,  $a < x_k < b$ , another damping  $\theta_k$  in the step may be needed to insure  $a < x_k < b$ . This can be stated in algorithmic form as follows

**Scheme 2.2.** (computing  $\theta_k$ )

If  $a < x_k + \tau_k \Delta x_k < b$ , then set  $\theta_k = 1$ .

Else choose  $\theta_k \in (0.99, 1)$ .

End if.

After computing the scaled step  $\Delta x_k$ , we set the trial step  $\omega_k = \theta_k \tau_k \Delta x_k$  and  $x_{k+1} = x_k + \omega_k$ . Estimates for the Lagrange multiplier  $\lambda_{k+1}$  is needed. To estimate the Lagrange multiplier  $\lambda_{k+1}$  we solve

$$\min_{\lambda \in R^m} \|\nabla f_{k+1} + \nabla C_{k+1} \lambda\|^2. \quad (2.3)$$

We test whether the point  $(x_{k+1}, \lambda_{k+1})$  will be accepted and taken as a next iterate. To test for that, a merit function is needed. The following augmented Lagrangian

$$\Phi(x, \lambda; \rho) = f(x) + \lambda^T C(x) + \rho \|C(x)\|^2, \quad (2.4)$$

is used as a merit function, where  $\rho > 0$  is the penalty parameter. The actual reduction in the merit function in moving from  $(x_k, \lambda_k)$  to  $(x_{k+1}, \lambda_{k+1})$  is defined as

$$Ared_k = \Phi(x_k, \lambda_k; \rho_k) - \Phi(x_{k+1}, \lambda_{k+1}; \rho_k). \quad (2.5)$$

The predicted reduction in the merit function is defined as

$$\begin{aligned} Pred_k = & -\nabla_x \ell(x_k, \lambda_k)^T \omega_k - \frac{1}{2} \omega_k^T \nabla_x^2 \ell_k \omega_k - \Delta \lambda_k^T (C_k + \nabla C_k^T \omega_k) \\ & + \rho_k [\|C_k\|^2 - \|C_k + \nabla C_k^T \omega_k\|^2], \end{aligned} \quad (2.6)$$

where  $\Delta \lambda_k = \lambda_{k+1} - \lambda_k$ .

## 2.2 Updating the penalty parameter $\rho_k$

The penalty parameter  $\rho_k$  is updated to ensure that

$$Pred_k \geq \frac{\rho_k}{2} \|C_k\|^2 - \|C_k + \nabla C_k^T \omega_k\|^2.$$

To update  $\rho_k$ , we use the scheme proposed in [10].

**Scheme 2.3.** (*computing  $\rho_k$* )

Set  $\rho_k = \rho_{k-1}$ .

If  $Pred_k < \frac{\rho_k}{2} [\|C_k\|^2 - \|C_k + \nabla C_k^T \omega_k\|^2]$ , then set

$$\rho_k = \frac{2[\nabla_x \ell(x_k, \lambda_k)^T \omega_k + \frac{1}{2} \omega_k^T \nabla_x^2 \ell_k \omega_k + \Delta \lambda_k^T (C_k + \nabla C_k^T \omega_k)]}{\|C_k\|^2 - \|C_k + \nabla C_k^T \omega_k\|^2} + \beta, \quad (2.7)$$

where  $\beta > 0$  is a small fixed constant.

## 2.3 Testing the Step and Updating $\delta_k$

The point  $(x_{k+1}, \lambda_{k+1})$  needs to be tested to determine whether it will be accepted. We do this by comparing  $Ared_k$  to  $Pred_k$ , as in the following scheme.

**Scheme 2.4.** (*testing  $(x_{k+1}, \lambda_{k+1})$  and updating  $\delta_k$* )

If  $\frac{Ared_k}{Pred_k} < \gamma_1$ , where  $0 < \gamma_1 < 1$ .

Reduce the trust-region radius by setting  $\delta_k = \alpha_1 \|\Delta x_k\|$ , where  $\alpha_1 \in (0, 1)$ .

Compute another trial point  $(x_{k+1}, \lambda_{k+1})$ .

Else if  $\gamma_1 \leq \frac{Ared_k}{Pred_k} < \gamma_2$ ,  $0 < \gamma_1 < \gamma_2 < 1$ , then

Accept the point  $(x_{k+1}, \lambda_{k+1})$ .

Set the trust-region radius:  $\delta_{k+1} = \max(\delta_k, \delta_{min})$ , where  $\delta_{min}$  is a fixed constant.

Else

Accept the point  $(x_{k+1}, \lambda_{k+1})$ .

Set the trust-region radius:  $\delta_{k+1} = \min\{\delta_{max}, \max\{\delta_{min}, \alpha_2 \delta_k\}\}$ , where  $\delta_{max}$  is a fixed constant, ( $\delta_{max} > \delta_{min}$ ) and  $\alpha_2 > 1$ .

End if.

Finally, the algorithm is terminated when  $\|D_k \nabla_x \ell_k\| + \|C_k\| \leq \varepsilon$ , for some  $\varepsilon > 0$ . A formal description of the proposed interior-point trust-region algorithm (IPTRA) for solving problem (1.1) is presented in Algorithm 1.

**Algorithm 1.** (IPTRA)

Step 0. (Initialization)

Given  $x_0 \in \mathbb{R}^n$  such that  $a < x_0 < b$ . Evaluate  $\lambda_0, D_0$ .

Set  $\rho_{-1} = 1$  and  $\beta = 0.1$ . Choose  $\varepsilon, \sigma, \alpha_1, \alpha_2, \gamma_1$ , and  $\gamma_2$  such that  $\varepsilon > 0, \sigma > 0, 0 < \alpha_1 < 1 < \alpha_2$ , and  $0 < \gamma_1 < \gamma_2 < 1$ . Choose  $\delta_{min}, \delta_{max}$ , and  $\delta_0$  such that  $\delta_{min} < \delta_{max}, \delta_0 \in [\delta_{min}, \delta_{max}]$ . Set  $k = 0$ .

Step 1. (Test for convergence)

If  $\|D_k \nabla_x \ell_k\| + \|C_k\| \leq \varepsilon$ , then terminate the algorithm.

Step 2. (Compute a trial step)

If  $\|C_k\| = 0$ , then

- a) Set  $s_k^n = 0$ .
- b) Compute the step  $\bar{s}_k^t$  by solving Subproblem (2.2)
- c) Set  $s_k = Z_k \bar{s}_k^t$ .

Else

a) Compute the normal component  $s_k^n$  by solving Subproblem (2.1).

b) If  $\|Z_k^T (D_k \nabla_x \ell_k + B_k s_k^n)\| = 0$ , then set  $\bar{s}_k^t = 0$ .

Else, compute  $\bar{s}_k^t$  by solving subproblem (2.2).

End if.

c) Set  $s_k = s_k^n + Z_k \bar{s}_k^t, \Delta x_k = D_k s_k$ .

End if.

Step 3. (Test for the box interiority)

- a) Compute the damping parameter  $\tau_k$  using Scheme 2.1.
- b) Set  $x_{k+1} = x_k + \tau_k \Delta x_k$ .
- c) Compute  $\theta_k$  according to Scheme 2.2

Step 4. (Compute Lagrange multipliers  $\lambda_{k+1}$ )

Compute  $\lambda_{k+1}$  by solving Subproblem (2.3).

Step 5. (Update the scaling matrix)

Compute  $D_{k+1}$ .

Step 6. (Update the penalty parameter  $\rho_k$ )

Updating  $\rho_k$  according to Scheme 2.3

Step 7. (Test the step and update the trust-region radius)

Test the step and update  $\delta_k$  according to Scheme 2.4

Step 8. Set  $k = k + 1$  and go to Step 1.

### 3 Numerical results

In this section, we report our numerical experience with the proposed trust-region algorithm IPTRA for solving Problem (1.1). Our program was written in MATLAB and run under MATLAB Version 7 with machine epsilon about  $10^{-16}$ .

Given a starting point  $x_0$  such that  $a < x_0 < b$ , we chose the initial trust-region radius  $\delta_0 = \max(\|s_0\|, \delta_{min})$ , where  $\delta_{min} = 10^{-3}$  and  $s_0$  is the full Cauchy step of the constraints  $C(x)$  at  $x_0$  (i.e.  $s_0 = -\frac{\nabla C_0^T \nabla C_0}{\nabla C_0^T \nabla^2 C_0 \nabla C_0} \nabla C_0^T C_0$ ). We chose the maximum trust-region radius to be  $\delta_{max} = 10^5 \delta_0$ . The values of the constants that are needed in step 0 of Algorithm IPTRA were set to be  $\gamma_1 = 10^{-4}$ ,  $\gamma_2 = 0.5$ ,  $\alpha_1 = 0.5$ ,  $\alpha_2 = 2$ ,  $\varepsilon = 10^{-8}$ ,  $\varepsilon_1 = 10^{-8}$ ,  $\varepsilon_2 = 10^{-8}$ .  $\theta = .9995$  and  $\beta = 0.1$ .

For computing the component of the trial steps, we have used the dogleg algorithm. Successful termination with respect to the proposed trust-region algorithm means that the termination condition of the algorithm is met with  $\varepsilon = 10^{-8}$ . On the other hand, unsuccessful termination means that the number of iterations is greater than 500 or the number of function evaluations is greater than 1000.

Numerical results obtained using Algorithm IPTRA have been reported and summarized in Tables (3.1) and (3.2). The problems which were tested in these tables were taken from Hock and Schittkowski [16]. The following abbreviations have been used:



HS : The number of problem as it is given in Hock and Schittkowski [16].  
 n : number of variables.  
 me : number of equality constraints.  
 mi : number of inequality constraints.  
 # Niter : number of iterations of Algorithm IPTRA.  
 # Nfunc : number of function evaluations of Algorithm IPTRA.  
 ngrad : value of  $\|D_k \nabla_x \ell_k\| + \|C_k\|$ .  
 # Fiter: number of iteration of Fletcher's algorithm [14].  
 # Ffunc: number of function evaluation of Fletcher's algorithm [14].

The numerical results of Algorithm IPTRA for some test problems of Hock and Schittkowski [16] at a feasible starting point with respect to the bounds have been listed. A comparison of our results with those obtained by Matlab is presented in Table (3.1).

A comparison of our numerical results against the corresponding results of Fletcher [14] at the same starting point indicated in Hock and Schittkowski is presented in Table (3.2). Solution obtained by the proposed algorithm are exactly identical to those given by Hock and Schittkowski.

## 4 Case Studies

In this section, four mechanical design problems are presented as case studies IPTRA algorithm.

### **Case 1.** *Design of a Pressure Vessel [17]*

*A cylindrical vessel is capped at both ends by hemispherical heads as shown in figure (4.1). The objective is to minimize the total cost, including the cost of the material, forming and welding. There are four design variables:  $T_s$  (thickness of the shell),  $T_h$  (thickness of the head),  $R$  (inner radius) and  $L$  (length of the cylindrical section of the vessel not including the head).  $T_s$  and  $T_h$  are integer multiples of 0.0625 inch, which are the available thicknesses of rolled steel plates, and  $R$  and  $L$  are continuous variables.*

Table 3.1: Numerical results of the Algorithm IPTRA for the Hock and Schittkowski's test problems.

problem	n	me	mi	starting point	Algorithm IPTRA		Matlab
					ngrad	$\frac{\#Niter}{\#Nfunc}$	$\frac{\#Niter}{\#Nfunc}$
HS1	2	0	1	(-2,1)	9.6006e-008	24/29	37/121
HS17	2	0	5	(0,1)	9.8648e-009	7/8	10/42
HS20	2	0	5	(0,1)	2.3282e-007	6/7	7/24
HS21	2	0	5	(5,2)	4.0984e-014	4/5	11/36
HS24	2	0	5	(1,0.5)	4.9898e-016	5/6	15/49
HS30	3	0	7	(2,1,1)	5.4610e-008	5/6	6/28
HS31	3	0	7	(2,2,0)	1.4414e-009	6/7	12/59
HS34	3	0	8	(5,2,3)	1.1253e-012	9/10	19/81
HS35	3	0	4	(0.5,0.5,0.5)	2.1551e-008	6/7	11/48
HS36	3	0	7	(10,10,10)	4.8587e-010	6/7	7/32
HS38	4	0	8	(3,1,3,1)	1.4350e-007	11/12	55/308
HS41	4	1	8	(0.5,0.5,0.5,1)	1.4168e-008	5/6	16/85
HS45	5	0	10	(0.5,0.7,1,2,3)	5.5541e-009	7/8	19/125
HS53	5	3	10	(2,2,2,2,2)	8.0960e-008	4/5	8/55
HS55	6	6	8	(0.5,1,1,0.5,1,2)	2.1991e-008	6/7	9/71
HS65	3	0	7	(1,1,0)	1.0674e-010	9/10	fail
HS66	3	0	8	(3,1.5,2)	2.5305e-009	8/9	14/60
HS71	4	1	9	(2,4,4,2)	1.2910e-010	6/7	8/46
HS74	4	3	10	(1,1,0,0)	4.8247e-007	15/16	15/79
HS75	4	3	10	(1,1,0,0)	1.4066e-009	16/17	10/55

Table 3.2: Numerical results of IPTRA and the corresponding results of Fletcher's algorithm.

problem	n	me	mi	Algorithm IPTRA		filterSD	
				# Niter / # Nfunc	# Fiter / # Ffunc		
HS6	2	1	0	16 / 28	4 / 8		
HS12	2	0	1	5/12	8/23		
HS19	2	0	6	7 / 8	6 / 7		
HS23	2	0	9	8 / 9	6 / 6		
HS26	3	1	0	19/ 23	5/61		
HS32	3	1	4	6 / 7	3 / 15		
HS39	4	2	0	9 / 10	20 / 121		
HS43	4	0	3	8/10	8/57		
HS60	3	1	6	7 / 8	3 / 35		
HS63	3	2	3	7 / 8	9 / 24		
HS80	5	2	10	6 / 7	6 / 30		
HS81	5	3	10	6 / 7	11 / 103		
HS93	6	0	8	10 / 17	4 / 213		

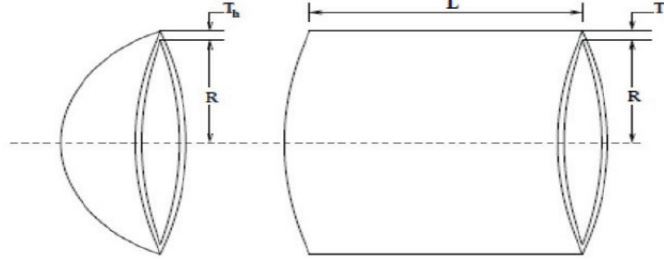


Figure 4.1: The pressure vessel design problem

Using the same notation given in [17], the problem can be stated as follows:

$$\text{minimize } f(x) = 0.6224x_1x_3x_4 + 1.7781x_2x_3^2 + 3.1661x_1^2x_4 + 19.84x_1^2x_3$$

subject to

$$g_1(x) = -x_1 + 0.0193x_3 \leq 0$$

$$g_2(x) = -x_2 + 0.00954x_3 \leq 0$$

$$g_3(x) = -\pi x_2^2 x_4 - (4/3)\pi x_3^3 + 1296000 + \leq 0$$

$$g_4(x) = x_4 - 240 \leq 0$$

$$0 \leq x_1, x_2 \leq 100,$$

$$10 \leq x_3, x_4 \leq 200.$$

A comparison of best solutions of this problem using different optimization techniques against ours is presented in Table (4.1). From Table (4.1), it can be seen that the solution found by IPTRA is better than the solutions found by other techniques which listed in the table.

Table 4.1: Comparison of the best solutions for the pressure vessel design problem.

Design variables	Kannan and Kramer (1994)[17]	Deb (1997)[9]	He and Wang (2007)[15]	Lobato and Steffen (2014)[18]	Algorithm IPTRA
$x_1$	1.125000	0.937500	0.812500	0.812500	0.7781686412897
$x_2$	0.625000	0.500000	0.437500	0.437500	0.3846491626309
$x_3$	58.29100	48.32900	42.09126	42.09127	40.3196187240987
$x_4$	43.69000	112.6790	176.7465	176.7466	200
$f$	7198.0428	6410.3811	6061.0777	6061.0778	5885.332773005870

**Case 2. Welded Beam Design [20]**

A welded beam is designed for minimum cost subject to constraints on shear stress ( $\tau$ ), bending stress in the beam ( $\sigma$ ) buckling load on the bar ( $P_c$ ), end deflection of the beam ( $\delta$ ), and side constraints. There are four design variables as shown in figure (4.2),  $h(x_1)$ ,  $l(x_2)$ ,  $t(x_3)$  and  $b(x_4)$ . The problem can be

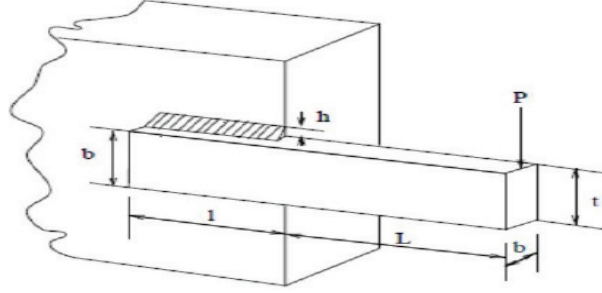


Figure 4.2: The welded beam design problem

stated as follows:

$$\text{Minimize } f(x) = 1.10471x_1^2x_2 + 0.04811x_3x_4(14.0 + x_2)$$

subject to

$$g_1(x) = \tau(x) - \tau_{max} \leq 0$$

$$g_2(x) = \sigma(x) - \sigma_{max} \leq 0$$

$$g_3(x) = x_1 - x_4 \leq 0$$

$$g_4(x) = 0.10471x_1^2 + 0.04811x_3x_4(14.0 + x_2) - 5.0 \leq 0$$

$$g_5(x) = 0.125 - x_1 \leq 0$$

$$g_6(x) = \delta - \delta_{max} \leq 0$$

$$g_7(x) = P - P_c \leq 0$$

$$\tau = \sqrt{(\tau_1)^2 + 2\tau_1\tau_2\frac{x_2}{2R} + (\tau_2)^2}$$

$$\tau_1 = \frac{P}{\sqrt{2}x_1x_2}$$

$$\tau_2 = \frac{MR}{J}$$

$$M = P(L + \frac{x_2}{2})$$

$$\begin{aligned}
R &= \sqrt{\frac{x_2^2}{4} + \left(\frac{x_1 + x_3}{2}\right)^2} \\
J &= 2\left\{\sqrt{2}x_1x_2\left[\frac{x_2^2}{12} + \left(\frac{x_1 + x_3}{2}\right)^2\right]\right\} \\
\sigma(x) &= \frac{6PL}{(x_4x_3^2)} \\
\delta(x) &= \frac{4PL^3}{(Ex_4x_3^3)} \\
P_c &= \frac{4.013E\sqrt{\frac{x_3^2x_4^6}{36}}}{L^2}\left(1 - \frac{x_3}{2L}\sqrt{\frac{E}{4G}}\right) \\
0.1 &\leq x_1, x_4 \leq 2 \\
0.1 &\leq x_2, x_3 \leq 10 \\
P &= 6000, L = 14, E = 30 \times 10^6, G = 12 \times 10^6 \\
\tau_{max} &= 13600, \sigma_{max} = 30000, \delta_{max} = 0.25
\end{aligned}$$

Table 4.2 presents a comparison between best solutions of different optimization techniques against ours for this problem. From which it can be seen that IPTRA solution is better than the solutions found by other techniques which listed in the table.

Table 4.2: Comparison of the best solutions for the welded beam design problem.

Design variables	Deb (1991)[8]	Coello (2000)[5]	He and Wang (2007)[15]	Lobato and Steffen (2014)[18]	Algorithm IPTRA
$x_1$	0.248900	0.208800	0.202369	0.208796	0.205727860241585
$x_2$	6.173000	3.420500	3.544214	3.412545	3.470389674407195
$x_3$	8.178900	8.997500	9.048210	8.910044	9.036980598594390
$x_4$	0.253300	0.210000	0.205723	0.210001	0.205727860244276
$f$	2.433116	1.748309	1.728024	1.7318117	1.724884179475869

**Case 3.** *Minimization the Weight of a Tension/Compression String*

This problem was proposed by Arora [1], Belegundu [3] and He and Wang [15]. It consists of minimizing the weight of a tension compression spring shown in figure (4.3) subject to constraints on minimum deflection, shear stress, surge frequency, limits on outside diameter and on design variables. The design variables are the mean coil diameter  $D$ , the wire diameter  $d$  and the number of active coils  $N$ .

The mathematical formulation of this problem can be described as follows:

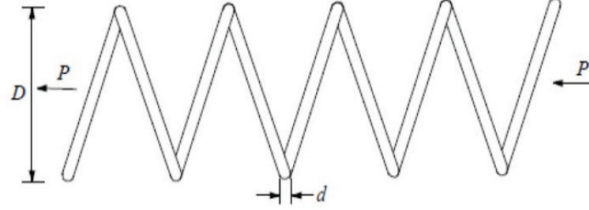


Figure 4.3: Tension/compression string problem

$$\begin{aligned} & \text{minimize } f(x) = (x_3 + 2)x_2x_1^2 \\ & \text{subject to} \end{aligned}$$

$$g_1(x) = 1 - \frac{x_2^3x_3}{71785x_1^4} \leq 0$$

$$g_2(x) = \frac{4x_2^2 - x_1x_2}{12566(x_2x_1^3 - x_1^4)} + \frac{1}{5108x_1^2} - 1 \leq 0$$

$$g_3(x) = 1 - \frac{140.45x_1}{x_2^2x_3} \leq 0$$

$$g_4(x) = \frac{x_1 + x_2}{1.5} - 1 \leq 0$$

$$0.05 \leq x_1 \leq 2$$

$$0.25 \leq x_2 \leq 1.3$$

$$2 \leq x_3 \leq 15.$$

Our solution for this problem is compared to the best solutions of different optimization techniques in Table (4.3), it can be seen that IPTRA solution is better than solutions found by other techniques listed in the table.

Table 4.3: Comparison of the best solutions for the tension/compression spring design problem.

Design variables	Belegundu (1982)[3]	Arora (1989)[1]	He and Wang (2007)[15]	Lobato and Steffen (2014)[18]	Algorithm IPTRA
$x_1$	0.050000	0.053396	0.051728	0.051744	0.051689061592032
$x_2$	0.315900	0.399180	0.357644	0.357754	0.356717752054532
$x_3$	14.25000	9.185400	11.244543	11.56132	11.288965032614222
$f$	0.012674	0.012730	0.012674	0.012789	0.012665232787753

**Case 4.** *Heat Exchanger Design [2]*

A fluid having a given flow rate  $W$  and specific heat  $C_p$  is heated from temperature  $T_0$  to  $T_3$  by passing three heat exchangers in series. In each heat exchanger (stage) the cold stream is heated by a hot fluid having the same flow rate  $W$  and specific heat  $C_p$  as the cold stream. The temperatures of the hot fluid entering the heat exchangers,  $t_{11}$ ,  $t_{21}$  and  $t_{31}$  and the overall heat transfer coefficients  $U_1$ ,  $U_2$ ,  $U_3$  of the exchangers are known constants. Optimal design involves minimizing the sum of the heat transfer areas of the three exchangers,  $A_T = A_1 + A_2 + A_3$ , as shown in figure (4.4).

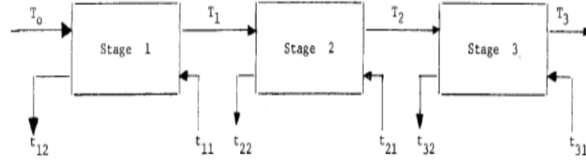


Figure 4.4: Three-stage heat exchanger system

The mathematical formulation of this problem can be described as follows [20]:

$$\text{minimize } A_T = A_1 + A_2 + A_3$$

subject to

$$g_1(x) = 0.0025(T_1 + t_{12}) - 1 \leq 0$$

$$g_2(x) = 0.0025(-T_1 + T_2 + t_{22}) - 1 \leq 0$$

$$g_3(x) = 0.01(-T_2 + t_{32}) - 1 \leq 0$$

$$g_4(x) = 100A_1 - A_1t_{12} + 833.33252T_1 - 83333.333 \leq 0$$

$$g_5(x) = A_2T_1 - A_2t_{22} - 1250T_1 + 1250T_2 \leq 0$$

$$g_6(x) = A_3T_2 - A_3t_{32} - 2500T_2 + 1250000 \leq 0$$

$$100 \leq A_1 \leq 10,000$$

$$1000 \leq A_i \leq 10,000, i = 2, 3$$

$$10 \leq T_i \leq 1000, i = 1, 2$$

$$10 \leq t_{i2} \leq 1000, i = 1, 2, 3.$$

From Table (4.4), it can be seen that the solution of the three-stage heat exchanger system problem found by IPTRA is almost the same by other competing technique (Avriel [2]).

Table 4.4: Comparison of the solutions for three-stage heat exchanger system problem.

Design variable	Avriel [2]	Algorithm IPTRA
$A_1$	567	579.306684436986
$A_2$	1357	1359.970668094694
$A_3$	5125	5109.970666971246
$T_1$	181	182.017699592019
$T_2$	295	295.601173303897
$t_{12}$	219	217.982300431680
$t_{22}$	286	286.416526324619
$t_{32}$	395	395.601173312338
$A_T$	7049	7049.248019502926

## 5 Conclusion remarks

In this paper, an interior point trust-region algorithm has been introduced to solve a general nonlinear programming problem. A Coleman-Li scaling matrix is used with an interior-point Newton method in the proposed algorithm. The reduced-Hessian technique is used to overcome the difficulty of having an infeasible trust-region subproblem and to simplify it.

A Matlab code of the proposed algorithm is implemented and tested against some existing codes. The results confirm the efficiency of the IPTRA algorithm. In addition to that, four case studies have been implemented to test the performance of the proposed algorithm where the results showed that the solution of the IPTRA algorithm is better than the best solutions of other techniques except for case 4 where the results were almost the same. We believe the proposed algorithm can be applied for solving real-world application problems efficiently.

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